

## Effect of Variable Viscosity on Natural Convection Flow Between Vertical Parallel Plates in the Presence of Heat Generation/Absorption

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### Authors' contributions

This work was carried out in collaboration between both authors. Both authors read and approved the final manuscript.

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## Abstract

The present article was aimed at investigating the effects of variable viscosity on natural convection flow between vertical parallel plates in the presence of heat generation/absorption. The nonlinear differential equations governing the flow were solved using Homotopy perturbation method. The impacts of the several governing parameters on the velocity and temperature profiles are presented graphically and values of skin friction, rate of heat transfer, mass flux and mean temperature for various values of physical parameters are presented through tables. In the course of computation, it was revealed that viscosity contributes to decrease velocity and hence reduced resistance to flow. It was also discovered that as the heat generation increases, fluid temperature and velocity increase, while it decrease with the increase in heat absorption. Finally, it was concluded that the skin friction on both plates increase as viscosity increases.

Keywords: Variable viscosity; natural convection; heat generation/absorption; Homotopy perturbation.

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## Nomenclatures

$g$  - acceleration due to gravity [ $ms^{-2}$ ]  
 $h$  - width of the channel [m]  
 $S$  - dimensionless heat generation/absorption parameter  
 $Q_0$  - heat generation/absorption coefficient [ $kgm^{-1}s^{-3}K^{-1}$ ]  
 $T^*$  - dimensional fluid temperature [K]  
 $T_w^*$  - channel wall temperature [K]  
 $T_0^*$  - temperature of the ambience [K]  
 $T$  - dimensionless fluid temperature  
 $u^*$  - dimensional velocity [ $ms^{-1}$ ]  
 $u$  - dimensionless velocity  
 $U$  - dimensional velocity of the moving plate [ $ms^{-1}$ ]  
 $y^*$  - co-ordinate perpendicular to the plate [m]  
 $y$  - dimensionless co-ordinate perpendicular to the plate  
 $Gr$  - Grashof number  
 $cp$  - specific heat at constant pressure [ $m^2s^{-2}K^{-1}$ ]  
 $\rho$  - density of the fluid [ $kgm^{-3}$ ]  
 $\alpha$  - thermal diffusivity [ $m^2s^{-1}$ ]  
 $p$  - embedding parameter  
 $\beta$  - coefficient of thermal expansion [ $K^{-1}$ ]  
 $\mu$  - coefficient of viscosity  
 $\nu$  - kinematic viscosity [ $m^2s^{-1}$ ]

## 1 Introduction

The study of natural convection flow in a vertical channel has received a great deal of attention due to its applications such as, engineering field, geophysics, oceanography and environmental problems. A detailed review of natural convection flow and heat transfer can be found in the following Abdou [1] studied the effect of radiation with temperature dependent viscosity and thermal conductivity on an unsteady stretching sheet through porous media. He concluded that velocity and temperature across the boundary layer increase with increasing viscosity variation parameter. Santana and Hazarika [2] examined the effects of variable viscosity and thermal conductivity on magnetohydrodynamics free convection and mass transfer flow over an inclined vertical surface in a porous medium with heat generation. They concluded that an increasing values of viscosity retard the velocity but enhances the temperature. Adel et al. [3] worked on the similarity solution for steady magnetohydrodynamics **Falkner-Skan** heat and mass transfer flow over a wedge in porous media considering thermal-diffusion and diffusion-thermo effects with variable viscosity and thermal conductivity. They discovered that the velocity of the fluid is found to increase with increase of the temperature dependent fluid viscosity. Makungu et al. [4] studied the effects of variable viscosity of nanofluid flow over a permeable wedge embedded in saturated porous medium with chemical reaction and thermal radiation. **Sher et al.** [5] studied squeezing nanofluid flow between two parallel plates under the influence of MHD and thermal radiation. They reported that temperature and concentration distributions vary inversely with Prandtl number, that is temperature distribution drop with large number of Prandtl number and rise for lesser values of Prandtl number. **Syed et al.** [6] considered a Bioconvection model for squeezing flow between parallel plates containing Gyrotactic microorganisms with impact of thermal radiation and heat generation/absorption. They concluded that the convergence of the homotopy method along with the variation of different physical parameters has been observed numerically. Ajibade and Tafida [7] studied viscous dissipation effect on steady natural convection Couette flow of heat generating

fluid in a vertical channel. The outcome of their study showed that fluid temperature and velocity increase with an increase in heat generation while it decreases with the increase in heat absorption. Hazarika and Gopal [8] analyzed the effects of variable viscosity and thermal conductivity on magnetohydrodynamics flow past a vertical plate. They observed **that the** velocity profile decreases with the increase of variable viscosity is not so prominent in case of temperature profile. Mohamed [9] examined dissipation and variable viscosity on steady magnetohydrodynamics free convective flow over a stretching sheet in presence of thermal radiation and chemical reaction. He discovered **that the** velocity decreases with an increase in viscosity parameter. Phukan and Hazarika [10] studied the effects of variable viscosity and thermal conductivity on magnetohydrodynamics free convective flow of micropolar fluid past a stretching plate through porous medium with radiation, heat generation and Joule heating. They reported that velocity decreases with the increase of the viscosity parameter. In another article, Noghrehabadi et al. [11] examined the effects of variable viscosity and thermal conductivity on natural convection of nanofluids past a vertical plate in a porous media. The outcomes showed **that an** increase of variable viscosity parameter increases the velocity profiles whereas decreases the concentration profiles. Moreover, variation of viscosity parameter does not show the significant effect on the temperature profiles. All the above mentioned studies did not consider the effect of heat generation/absorption.

The study of heat generation/absorption in moving fluids is important in several physical problems dealing with chemical reactions and those concerned with dissociating fluids. Possible heat generation effects may alter the temperature distribution and therefore, the particle deposition rate. **Sher et al.** [12] studied the rotating flow of MHD carbon nanotubes over a stretching sheet with the impact of non-linear thermal radiation and heat generation/absorption. They discovered that the rate of heat is enhanced as the heat generation/absorption value is increased. Consequently, He further discovered that the thermal thickness of boundary film is a function of heat generation/absorption. Chamkha and Camille [13] solved hydromagnetic flow with heat and mass transfer over a flat plate in the presence of heat generation or absorption and thermophoresis. **Mohammad et al.** [14] studied entropy generation on nanofluid thin film flow of Eyring-powell fluid with thermal radiation and MHD effect on an unsteady porous stretching sheet. They outcome of their study showed that the growing behavior of Prandtl number increases the surface temperature where the opposite effect is found for an unsteady parameter, that is, the larger values of an unsteadiness reduce the surface temperature. Natural convection with heat generation along a uniformly heat vertical wavy surface have been demonstrated by Molla et al. [15]. Veena et al. [16] worked on heat transfer characteristics in the laminar boundary layer flow of a viscoelastic fluid over a linearly stretching continuous surface with variable wall temperature subjected to suction or blowing. Jha and Ajibade [17] considered the case of unsteady free convective Couette flow of heat generating/absorbing fluid. **The outcome of their study showed that the** skin friction increased as the external heating/cooling increases, likewise an increase in heat absorption increases the rate of heat transfer on the moving plate and decreases the rate of heat transfer on the stationary plate.

The objective of this study is to investigate the effect of variable viscosity on natural convection flow between vertical parallel plates in the presence of heat generation/absorption. **The equations** governing the flow have some non linear terms in them so that obtaining closed form solution is a daunting task. Such problems can therefore be approached by numerical schemes or some approximate solution methods. One of the efficient methods is the perturbation method. However, solutions obtained by perturbation method are restricted to small perturbation parameters, therefore to overcome this restriction, another method called Homotopy perturbation method was introduced.

He [18] was first studied to solve linear, non-linear and **coupled** problems in partial or ordinary form. He [19] studied a coupling method of a Homotopy technique and a perturbation technique for non-linear problems. In another article, He [20] studied a new non linear analytical technique using Homotopy perturbation methods. Da-Hua [21] studied Homotopy perturbation method for nonlinear oscillators.

From the computational point of view it is identified and proved beyond all doubts that the Homotopy perturbation method is very efficient and powerful tool for solving coupled and nonlinear system of differential equations. In this paper, we extend the work of Jha and Ajibade [17] to investigate the effect of variable viscosity on natural convection flow through a vertical parallel plates in the presence of heat generation/absorption. The velocity and temperature field are obtained and discussed for some carefully selected values of the flow parameters.

## 2 Mathematical Analysis

We considers a steady natural convection flow of an incompressible viscous fluid in a vertical channel of width  $h$ . The flow is assumed to be in the  $x^*$  - direction which is taken vertically along one of the plates while  $y^*$  - axis is taken normal to it. The second is placed  $h$  distance away from the first. The temperature of the fluid and one of the channel plates are kept at  $T_0$  while the temperature of the plate  $y^* = 0$  is raised or fell to  $T_w$  and thereafter maintained constant. Also, the plate  $y^* = 0$  moves in its own plane impulsively at a uniform velocity  $u^* = U$  while the other plate remains at rest. The flow configuration and coordinates system is shown in figure 1.

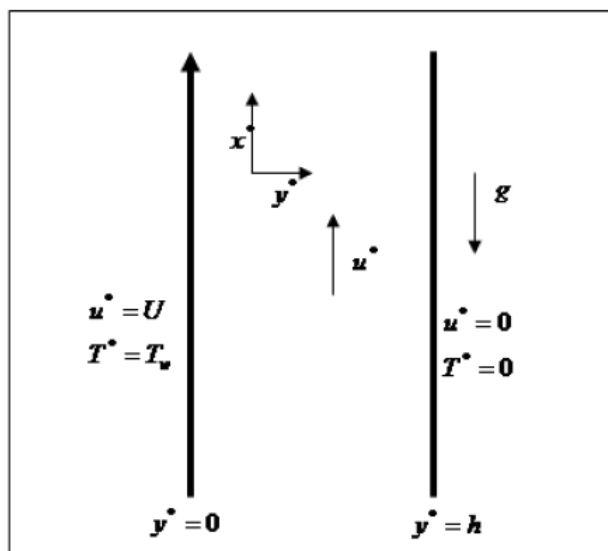


Fig. 1. Schematic diagram of the problem

Under the usual assumption of Boussinesq's approximation, the governing equations of the continuity, momentum and energy are as follows:

$$\frac{du^*}{dx^*} = 0, \quad (1)$$

$$\frac{1}{\rho} \frac{d}{dy^*} \left( \mu^* \frac{du^*}{dy^*} \right) + g\beta(T^* - T_0) = 0, \quad (2)$$

$$\alpha \frac{d^2 T^*}{dy^{*2}} - \frac{Q_0}{\rho c p} (T^* - T_0) = 0. \quad (3)$$

The viscosity of the working fluid is assumed to vary linearly with temperature as follows

$$\mu^* = \mu_0(1 - \lambda^*(T^* - T_0))$$

while the boundary conditions are:

$$\begin{aligned} u^* = U, \quad T^* = T_w \quad \text{at} \quad y^* = 0, \\ u^* = 0, \quad T^* = T_0 \quad \text{at} \quad y^* = h. \end{aligned} \quad (4)$$

Due to the nature of the quantities that are given in different dimensions, we introduce some dimensionless quantities that can transform the governing equations **and their boundary** conditions into dimensionless form. The dimensionless quantities used in equations (1) - (3) and the boundary condition (4) are:

$$\begin{aligned} y = \frac{y^*}{h}, \quad u = \frac{u^*}{U}, \quad T = \frac{T^* - T_0}{T_w - T_0}, \quad S = \frac{Q_0 h^2}{k}, \\ Gr = \frac{g \beta h^2 (T_w - T_0)}{v U}, \quad \lambda = \lambda^* (T_w - T_0). \end{aligned} \quad (5)$$

By using the dimensionless quantities, the governing equations and the boundary conditions are transformed into non-dimensional form as

$$\frac{du}{dx} = 0, \quad (6)$$

$$(1 - \lambda T) \frac{d^2 u}{dy^2} - \lambda \frac{du}{dy} \cdot \frac{dT}{dy} + Gr(1 - \lambda T)T = 0, \quad (7)$$

$$\frac{d^2 T}{dy^2} - ST = 0. \quad (8)$$

And the boundary conditions are:

$$\begin{aligned} u = 1, \quad T = 1 \quad \text{at} \quad y = 0, \\ u = 0, \quad T = 0 \quad \text{at} \quad y = 1. \end{aligned} \quad (9)$$

## 2.1 Homotopy Perturbation Method

In order to illustrate the basic ideas of the Homotopy Perturbation Method (HPM), we consider the following nonlinear differential equation

$$A(u) - f(r) = 0, \quad r \in \Omega, \quad (10)$$

with the boundary conditions

$$B(u, \frac{\partial u}{\partial n}) = 0 \quad r \in \Gamma, \quad (11)$$

where  $A$  is a general differential operator,  $B$  is a boundary operator,  $f(r)$  is known analytical function and  $\Gamma$  is the boundary of the domain  $\Omega$ , respectively. Generally speaking, the operator  $A$  can be divided into two parts which are  $L$  and  $N$ , where  $L$  is linear part and  $N$  is nonlinear part. Therefore (10) can be written as:

$$L(u) + N(u) - f(r) = 0, \quad r \in \Omega, \quad (12)$$

By the homotopy techniques, we construct a homotopy as follows  $v(r, p) : \Omega \times [0, 1] \rightarrow R$  which satisfies:

$$H(v, p) = (1 - p)[L(v) - L(u_0)] + p[A(v) - f(r)] = 0, \quad (13)$$

in equation (13),  $p \in [0, 1]$  is an embedding parameter, while  $u_0$  is an initial approximation of equation (10), which satisfies the boundary conditions. Clearly from eqn (13), we have

$$H(v, 0) = L(v) - L(u_0) = 0, \tag{14}$$

$$H(v, 1) = A(v) - f(r) = 0. \tag{15}$$

We can assume that the solution of equation (13) can be written as a power series in  $p$ :

$$v = v_0 + pv_1 + p^2v_2 + \dots, \tag{16}$$

setting  $p = 1$  gives the approximate solution of eqn (10) as

$$u = \lim_{p \rightarrow 1} v = v_0 + v_1 + v_2 + \dots \tag{17}$$

Applying the Homotopy perturbation technique to solve the governing equations in the present problem, we construct a convex Homotopy on eqs. (7) and (8) to get

$$H(u, p) = (1 - p) \left[ \frac{d^2 u}{dy^2} \right] + p \left[ \frac{d^2 u}{dy^2} + \lambda T \frac{d^2 u}{dy^2} + \lambda \frac{du}{dy} \cdot \frac{dT}{dy} - GrT + \lambda GrT^2 \right] = 0, \tag{18}$$

$$H(T, p) = (1 - p) \left[ \frac{d^2 T}{dy^2} \right] + p \left[ \frac{d^2 T}{dy^2} - ST \right] = 0, \tag{19}$$

using infinite series (18) and (19) to define  $u$  and  $T$  as follows

$$\begin{aligned} u &= u_0 + pu_1 + p^2u_2 + \dots, \\ T &= T_0 + pT_1 + p^2T_2 + \dots \end{aligned} \tag{20}$$

Substituting eqn. (20) into eqns. (18) and (19), we have

$$\begin{aligned} \frac{d^2 u_0}{dy^2} + p \frac{d^2 u_1}{dy^2} + p^2 \frac{d^2 u_2}{dy^2} + p^3 \frac{d^2 u_3}{dy^2} + \dots &= p\lambda T_0 \frac{d^2 u_0}{dy^2} + p^2 \left[ \lambda T_0 \frac{d^2 u_1}{dy^2} + \lambda T_1 \frac{d^2 u_0}{dy^2} \right] \\ &+ p^3 \left[ \lambda T_0 \frac{d^2 u_2}{dy^2} + \lambda T_2 \frac{d^2 u_0}{dy^2} + \lambda T_1 \frac{d^2 u_1}{dy^2} \right] + \dots \\ &+ p\lambda \frac{du_0}{dy} \cdot \frac{dT_0}{dy} + p^2 \left[ \frac{du_0}{dy} \cdot \frac{dT_1}{dy} + \lambda \frac{du_1}{dy} \cdot \frac{dT_0}{dy} \right] \\ &+ p^3 \left[ \lambda \frac{du_0}{dy} \cdot \frac{dT_2}{dy} + \lambda \frac{du_2}{dy} \cdot \frac{dT_0}{dy} + \lambda \frac{du_1}{dy} \cdot \frac{dT_1}{dy} \right] + \dots \\ &- pGrT_0 - p^2GrT_1 - p^3GrT_2 - \dots \\ &+ p\lambda GrT_0^2 + p^2 [2\lambda GrT_0T_1] \\ &+ p^3 [2\lambda GrT_0T_2 + \lambda GrT_1^2] + \dots \end{aligned} \tag{21}$$

$$\frac{d^2 T_0}{dy^2} + p \frac{d^2 T_1}{dy^2} + p^2 \frac{d^2 T_2}{dy^2} + p^3 \frac{d^2 T_3}{dy^2} + \dots = pST_0 + p^2ST_1 + p^3ST_2 + \dots \tag{22}$$

By comparing the coefficient of  $p^0$ ,  $p^1$ ,  $p^2$  and  $p^3$  of eqns. (21) and (22), we have

$$P^0 : \frac{d^2 u_0}{dy^2} = 0, \tag{23}$$

$$P^0 : \frac{d^2 T_0}{dy^2} = 0, \tag{24}$$

$$P^1 : \frac{d^2 u_1}{dy^2} = \lambda T_0 \frac{d^2 u_0}{dy} + \lambda \frac{du_0}{dy} \cdot \frac{dT_0}{dy} - GrT_0 + \lambda GrT_0^2, \tag{25}$$

$$P^1 : \frac{d^2 T_1}{dy^2} = ST_0, \tag{26}$$

$$P^2 : \frac{d^2 u_2}{dy^2} = \lambda T_0 \frac{d^2 u_1}{dy^2} + \lambda T_1 \frac{d^2 u_0}{dy^2} + \lambda \frac{du_0}{dy} \cdot \frac{dT_1}{dy} + \lambda \frac{du_1}{dy} \cdot \frac{dT_0}{dy} - GrT_1 + 2\lambda GrT_0T_1, \tag{27}$$

$$P^2 : \frac{d^2 T_2}{dy^2} = ST_1, \tag{28}$$

$$P^3 : \frac{d^2 u_3}{dy^2} = \lambda T_0 \frac{d^2 u_2}{dy^2} + \lambda T_2 \frac{d^2 u_0}{dy^2} + \lambda T_1 \frac{d^2 u_1}{dy^2} + \lambda \frac{du_0}{dy} \cdot \frac{dT_2}{dy} + \lambda \frac{du_2}{dy} \cdot \frac{dT_0}{dy} + \lambda \frac{du_1}{dy} \cdot \frac{dT_1}{dy} - GrT_2 + 2\lambda GrT_0T_2 + \lambda GrT_1^2, \tag{29}$$

$$P^3 : \frac{d^2 T_3}{dy^2} = ST_2. \tag{30}$$

:  
:  
:

The boundary conditions are transformed also as

$$\begin{aligned} T_0(0) = 1, \quad T_1(0) = T_2(0) = T_3(0) = \dots = 0, \\ T_0(1) = T_1(1) = T_2(1) = \dots = 0, \\ u_0(0) = 1, \quad u_1(0) = u_2(0) = u_3(0) = \dots = 0, \\ u_0(1) = u_1(1) = u_2(1) = \dots = 0. \end{aligned} \tag{31}$$

Since the zeroth order of the Homotopy gives a linear ordinary differential equations, it is easily solvable without making recourse to initial guess. Therefore solving eqs. (23) and (24) and applying the boundary conditions  $T_0(0) = 1$  and  $T_0(1) = 0$ ,  $u_0(0) = 1$  and  $u_0(1) = 0$ , we obtain eqs. (32) and (33) as

$$u_0 = A_1 y + A_2, \tag{32}$$

$$T_0 = B_1 y + B_2. \tag{33}$$

Solving eqs. (25) and (26) and applying the boundary conditions  $T_1(0) = 0$  and  $T_1(1) = 0$ ,  $u_1(0) = 0$  and  $u_1(1) = 0$ , we obtain eqs. (34) and (35) as

$$u_1 = \frac{\lambda y^2}{2} + \lambda Gr \left[ \frac{y^2}{2} - \frac{y^3}{3} + \frac{y^4}{12} \right] - Gr \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] + A_3 y + A_4, \tag{34}$$

$$T_1 = S \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] + B_3 y + B_4. \quad (35)$$

Solving eqs. (27) and (28) and applying the boundary condition  $T_2(0) = 0$  and  $T_2(1) = 0$ ,  $u_2(0) = 0$  and  $u_2(1) = 0$ , we obtain eqs. (36) and (37) as

$$\begin{aligned} u_2 = & \lambda^2 \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] + \lambda^2 Gr \left[ \frac{y^2}{2} - \frac{y^3}{2} + \frac{y^4}{4} - \frac{y^5}{20} \right] - \lambda Gr \left[ \frac{y^2}{2} - \frac{y^3}{3} + \frac{y^4}{12} \right] \\ & - \lambda S \left[ \frac{y^3}{6} - \frac{y^4}{24} \right] + \frac{\lambda S y^2}{6} - \frac{\lambda^2 y^3}{6} - \lambda^2 Gr \left[ \frac{y^3}{6} - \frac{y^4}{24} + \frac{y^5}{60} \right] - \frac{\lambda Gr y^2}{6} \\ & + \lambda Gr \left[ \frac{y^3}{6} - \frac{y^4}{24} \right] + \frac{\lambda^2 y^2}{4} + \frac{\lambda^2 Gr y^2}{8} - Gr S \left[ \frac{y^4}{24} - \frac{y^5}{120} \right] + \frac{Gr S y^3}{18} \\ & + 2\lambda Gr S \left[ \frac{y^4}{24} - \frac{y^5}{30} + \frac{y^6}{180} \right] - \frac{2\lambda Gr S}{3} \left[ \frac{y^3}{6} - \frac{y^4}{12} \right] + A_5 y + A_6, \end{aligned} \quad (36)$$

$$T_2 = S^2 \left[ \frac{y^4}{24} - \frac{y^5}{120} \right] - \frac{S^2 y^3}{18} + B_5 y + B_6. \quad (37)$$

Solving eqs. (29) and (30) and applying the boundary condition  $T_2(0) = 0$  and  $T_2(1) = 0$ ,  $u_2(0) = 0$  and  $u_2(1) = 0$ , we obtain eqs. (38) and (39) as

$$\begin{aligned} u_3 = & \lambda^3 \left[ \frac{y^2}{2} - \frac{y^3}{3} + \frac{y^4}{12} \right] + \lambda^3 Gr \left[ \frac{y^2}{2} - \frac{2y^3}{3} + \frac{y^4}{2} - \frac{y^5}{5} + \frac{y^6}{30} \right] - \lambda^3 \left[ \frac{y^3}{6} - \frac{y^4}{12} \right] \\ & - \lambda^2 Gr \left[ \frac{y^2}{2} - \frac{y^3}{2} + \frac{y^4}{4} - \frac{y^5}{20} \right] + \frac{\lambda^2 S}{3} \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] - \lambda^2 S \left[ \frac{y^3}{6} - \frac{y^4}{8} + \frac{y^5}{40} \right] \\ & - \lambda^3 Gr \left[ \frac{y^3}{6} - \frac{y^4}{6} + \frac{y^5}{15} - \frac{y^6}{90} \right] + \lambda^2 Gr \left[ \frac{y^3}{6} - \frac{y^4}{8} + \frac{y^5}{40} \right] + \frac{\lambda^3}{2} \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] \\ & - \frac{\lambda^2 Gr}{3} \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] + \frac{\lambda^3 Gr}{4} \left[ \frac{y^2}{2} - \frac{y^3}{6} \right] + \frac{\lambda S^2 y^2}{72} + \frac{\lambda Gr S}{3} \left[ \frac{y^3}{6} - \frac{y^4}{12} \right] \\ & - \lambda Gr S \left[ \frac{y^4}{24} - \frac{y^5}{30} + \frac{y^6}{180} \right] + 2\lambda^2 Gr S \left[ \frac{y^4}{24} - \frac{7y^5}{120} + \frac{y^6}{36} - \frac{y^7}{252} \right] - \frac{\lambda S^2 y^2}{90} \end{aligned}$$



$$\begin{aligned}
 & -\frac{2\lambda^2 GrS}{3} \left[ \frac{y^3}{6} - \frac{y^4}{6} + \frac{y^5}{20} \right] + \lambda^2 S \left[ \frac{y^4}{24} - \frac{y^5}{120} \right] - \lambda GrS \left[ \frac{y^4}{24} - \frac{y^5}{30} + \frac{y^6}{180} \right] \\
 & + \lambda^2 GrS \left[ \frac{y^4}{24} - \frac{7y^5}{120} + \frac{y^6}{36} - \frac{y^7}{252} \right] - \frac{\lambda^2 Sy^3}{18} - \frac{\lambda^2 GrS}{3} + \left[ \frac{y^3}{6} - \frac{y^4}{6} + \frac{y^5}{20} \right] \\
 & + \frac{\lambda GrS}{3} \left[ \frac{y^3}{6} - \frac{y^4}{12} \right] - \lambda S^2 \left[ \frac{y^5}{120} - \frac{y^6}{720} \right] - \lambda^3 \left[ \frac{y^3}{6} - \frac{y^4}{24} \right] + \frac{\lambda^2 Gry^3}{18} - \frac{\lambda^3 y^3}{12} \\
 & - \lambda^3 Gr \left[ \frac{y^3}{6} - \frac{y^4}{8} + \frac{y^5}{20} - \frac{y^6}{120} \right] + \lambda^2 S \left[ \frac{y^4}{24} - \frac{y^5}{120} \right] + \lambda^2 Gr \left[ \frac{y^3}{6} - \frac{y^4}{12} + \frac{y^5}{60} \right] \\
 & + \lambda^3 Gr + \left[ \frac{y^4}{24} - \frac{y^5}{60} + \frac{y^6}{360} \right] - \lambda^2 Gr \left[ \frac{y^4}{24} - \frac{y^5}{120} \right] + \lambda GrS \left[ \frac{y^5}{120} - \frac{y^6}{720} \right] \\
 & + \frac{\lambda^3 y^4}{24} - \frac{\lambda^3 Gry^3}{24} - \frac{\lambda^2 Sy^3}{18} - 2\lambda^2 GrS \left[ \frac{y^5}{120} - \frac{y^6}{180} + \frac{y^7}{1260} \right] - \frac{\lambda GrSy^4}{72} \\
 & + \frac{2\lambda^2 GrS}{3} \left[ \frac{y^4}{24} - \frac{y^5}{60} \right] + \frac{5\lambda^3 y^2}{24} + \frac{9\lambda^3 Gry^2}{80} - \frac{7\lambda^2 Gry^2}{48} + \frac{\lambda^2 Sy^2}{48} + \frac{\lambda GrSy^2}{90} \\
 & - \frac{\lambda^2 GrSy^2}{72} + \lambda^2 S \left[ \frac{y^4}{12} - \frac{y^5}{40} \right] - \frac{\lambda^2 Sy^3}{18} + \lambda^2 GrS \left[ \frac{y^4}{12} - \frac{3y^5}{40} + \frac{y^6}{36} - \frac{y^7}{252} \right] \\
 & - \frac{\lambda^2 GrS}{3} \left[ \frac{y^3}{6} - \frac{y^4}{12} + \frac{y^5}{60} \right] - \lambda GrS \left[ \frac{y^4}{12} - \frac{y^5}{20} + \frac{y^6}{120} \right] - \frac{\lambda^2 S}{2} \left[ \frac{y^3}{6} - \frac{y^4}{24} \right] \\
 & + \frac{\lambda GrS}{3} \left[ \frac{y^3}{3} - \frac{y^4}{12} \right] - \frac{\lambda GrSy^2}{18} + \frac{\lambda^2 Sy^2}{12} - \frac{\lambda^2 GrS}{4} \left[ \frac{y^3}{6} - \frac{y^4}{24} \right] + \frac{\lambda^2 GrS}{24} \\
 & - GrS^2 \left[ \frac{y^6}{720} - \frac{y^7}{5040} \right] + \frac{GrS^2 y^3}{360} - \frac{GrS^2 y^3}{270} - \frac{\lambda GrS^2}{9} \left[ \frac{y^5}{20} - \frac{y^6}{30} \right] - \frac{\lambda^2 Sy^3}{18} \\
 & + \lambda GrS^2 \left[ \frac{y^6}{120} - \frac{y^7}{252} + \frac{y^8}{2016} \right] + 2\lambda GrS^2 \left[ \frac{y^6}{720} - \frac{y^7}{840} + \frac{y^8}{6720} \right] + \frac{\lambda GrS^2 y^4}{108} \\
 & - \frac{2\lambda GrS^2}{3} \left[ \frac{y^5}{40} - \frac{y^6}{180} \right] + A_7 y + A_8,
 \end{aligned} \tag{38}$$

$$T_3 = S^3 \left[ \frac{y^6}{720} - \frac{y^7}{5040} \right] - \frac{S^3 y^5}{360} + \frac{S^3 y^3}{270} + B_7 y + B_8. \tag{39}$$

Eqns (32) - (39) gives the expressions for the velocity and temperature as

$$u = u_0 + u_1 + u_2 + u_3 + \dots, \tag{40}$$

$$T = T_0 + T_1 + T_2 + T_3 + \dots \tag{41}$$

where,

$$\begin{aligned}
 A_1 = B_1 = -1, \quad A_2 = B_2 = 1, \quad A_3 = \frac{Gr}{3} - \frac{\lambda}{2} - \frac{\lambda Gr}{4}, \quad B_3 = -\frac{S}{3}, \\
 A_4 = B_4 = A_6 = B_6 = A_8 = B_8 = 0, \\
 A_5 = -\frac{5\lambda^2}{12} - \frac{9\lambda^2 Gr}{40} + \frac{7\lambda Gr}{24} - \frac{\lambda S}{24} - \frac{GrS}{45} + \frac{\lambda GrS}{36}, \quad B_5 = \frac{S^2}{45}, \\
 A_7 = -\frac{3\lambda^3}{8} - \frac{151\lambda^3 Gr}{720} + \frac{193\lambda^2 Gr}{720} - \frac{2\lambda^2 S}{45} - \frac{13\lambda GrS}{720} + \frac{1673\lambda^2 GrS}{70560} \\
 + \frac{\lambda S^2}{240} + \frac{2GrS^2}{945} - \frac{\lambda GrS^2}{270}, \quad B_7 = -\frac{2S^3}{945}.
 \end{aligned}$$

To obtain the skin friction and rate of heat transfer at the surfaces of the channel boundaries, the expressions for velocity and temperature are differentiated with respect to  $y$ , that is  $\tau = (1 - \lambda T) \frac{du}{dy}|_{y=0, y=1}$  and  $Nu = \frac{dT}{dy}|_{y=0, y=1}$  so that,

$$\begin{aligned} \frac{du}{dy}|_{y=0} &= -1 + A_3 + A_5, \\ \tau_0 &= (1 - \lambda T) \frac{du}{dy}|_{y=0}, \end{aligned} \tag{42}$$

$$\begin{aligned} \frac{du}{dy}|_{y=1} &= -1 + \lambda - \frac{Gr}{2} + A_3 + \frac{\lambda^2}{2} + \frac{\lambda^2 Gr}{12} + \frac{GrS}{24} - \frac{2\lambda GrS}{45} + A_5, \\ \tau_1 &= (1 - \lambda T) \frac{du}{dy}|_{y=1}, \end{aligned} \tag{43}$$

$$\frac{dT}{dy}|_{y=0} = -1 + B_3 + B_5, \tag{44}$$

$$\frac{dT}{dy}|_{y=1} = -1 + \frac{S}{2} + B_3 - \frac{S^2}{24} + B_5, \tag{45}$$

To obtain the mass flux  $Q$ , we have

$$Q = \frac{1}{2} + \frac{\lambda}{6} - \frac{\lambda Gr}{45} - \frac{Gr}{8} + \frac{A_3}{2} + \frac{\lambda^2}{6} + \frac{4\lambda^2 Gr}{45} + \frac{GrS}{144} - \frac{\lambda GrS}{840} + \frac{\lambda S}{45} + \frac{A_5}{2}, \tag{46}$$

and mean temperature  $\theta_m$ , we have

$$\theta_m = \frac{\int_0^1 uT(y)dy}{\int_0^1 u(y)dy}, \tag{47}$$

### 3 Results and discussion

The present work analyses the effects of variable viscosity on natural convection flow between vertical parallel plates in the presence of heat generation/absorption using Homotopy perturbation method. The velocity and temperature fields are presented graphically in figures 2-5 for various values of Grashof number ( $Gr$ ), heat generation/absorption parameter ( $S$ ) and variable viscosity ( $\lambda$ ). For the purpose of this discussion, the parameters of interest are carefully selected between  $1 \leq Gr \leq 10$ ,  $-2 \leq S \leq 2$  and  $-1 \leq \lambda \leq 1$ .

Figures 2 and 3 display temperature and velocity profiles for different values of heat generation/absorption parameter ( $S$ ). It should be noted that positive values of  $S$  signifies heat absorption while negative values of  $S$  signifies heat generation. It is seen from the figures that as the heat generation ( $S < 0$ ) increases, fluid temperature and velocity increase while, fluid temperature and velocity decrease with increase in heat absorption ( $S > 0$ ). Increasing the heat generation parameter causes the fluid temperature to increase and it strengthens the convection current within the channel which in turn increases the fluid velocity. In addition, fluid temperature drop as a result of increasing the heat absorption parameter and the thermal boundary layer becomes thinner thereby reduces the velocity distribution of the fluid as shown in figure 3.

Figure 4 shows the influence of thermal buoyancy parameter ( $Gr$ ) on the fluid velocity for fixed values of heat generation/absorption parameter ( $S$ ) and variable viscosity parameter ( $\lambda$ ). It is clear from this figure, the velocity profile increases with increases in the values of thermal buoyancy. Increasing the buoyancy parameter is made possible by decreasing the fluid viscosity which lead to thickening of the momentum boundary layer and hence an increase in velocity with growing  $Gr$ . Figure 5 depict the effect of viscosity parameter ( $\lambda$ ) on the velocity profile for fixed values of heat

generation/absorption parameter ( $S$ ) and Grashof number ( $Gr$ ). It is seen from the figure that velocity decreases with the increase of the viscosity parameter and hence reduced resistance to flow.

The skin friction on both plate is simulated and presented in Table 1. From Table 1 it is evident to show that growing buoyancy parameter, heat generation as well as viscosity have tendency to increase the skin friction on both plates. However, heat absorption contributes a decrease in the skin friction and this due to velocity decrease caused by increasing heat absorption which consequently leads to decrease in the skin friction on both plates.

Table 2 reveals the numerical values of rate of heat transfer on both plates. A general view of this table indicates that growing buoyancy parameter, heat generation as well as viscosity leads to a significant changes in the rate of heat transfer, this can be attributed to decrease on the heated plate while the opposite trend is observed on the cold plate. Furthermore, heat absorption leads to increase in the heat transfer on the heated plate.

Table 3 presents the mass flux  $Q$  within the channels. It is clearly seen that the mass flux increases with the increase in heat generation and decreases with increasing heat absorption. The table further shows that growing buoyancy parameter and viscosity leads to increase the mass flux.

Table 4 shows the numerical values of mean temperature  $\theta_m$ . It is observed that with the increase in heat generation, mean temperature decreases and the reverse trend is observed in heat absorption.

To validate this problem, we compare our results obtained for temperature as well as velocity are in good agreement with those of Jha and Ajibade [17] as shown in table 5 which shows that the Homotopy perturbation method is an efficient tool for solving coupled and nonlinear system of differential equations.

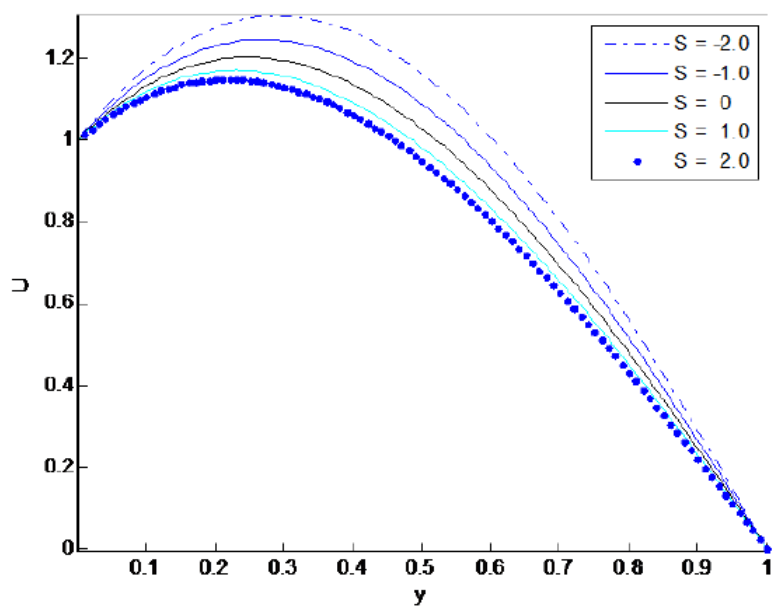


Fig. 2. Velocity profile for different values of  $S$  ( $Gr = 8.0, \lambda = -0.2$ )

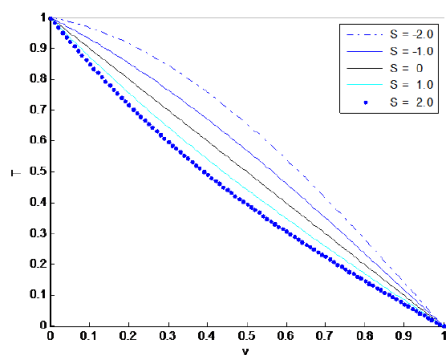


Fig. 3. Temperature profile for different values of  $S$  ( $Gr = 8.0, \lambda = -0.2$ )

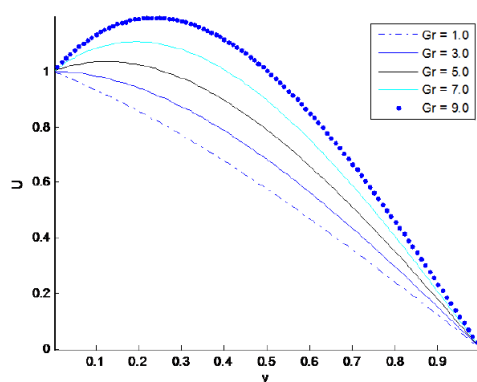


Fig. 4. velocity profile for different values of  $Gr$  ( $S = 2.0, \lambda = -0.2$ )

Table 1. Estimated numerical values of skin friction  $\tau_0$  and  $\tau_1$

S	$Gr = 5.0, \lambda = -0.3$		$Gr = 8.0, \lambda = -0.1$	
	$\tau_0$	$\tau_1$	$\tau_0$	$\tau_1$
-1	0.98240	2.23681	2.04270	2.60022
-0.5	0.89122	2.16944	1.93499	2.51369
0.5	0.70886	2.03472	1.71958	2.34064
1	0.61768	1.96736	1.61187	2.25411

Table 2. Estimated numerical values of rate of heat transfer  $Nu_0$  and  $Nu_1$

S	$Gr = 5.0, \lambda = -0.3$		$Gr = 8.0, \lambda = -0.1$	
	$Nu_0$	$Nu_1$	$Nu_0$	$Nu_1$
-1	0.64444	1.18611	0.64313	1.93121
-0.5	0.82778	1.08819	0.81146	1.96662
0.5	1.16111	0.92153	1.16010	1.99301
1	1.31111	0.85278	1.29000	2.03011

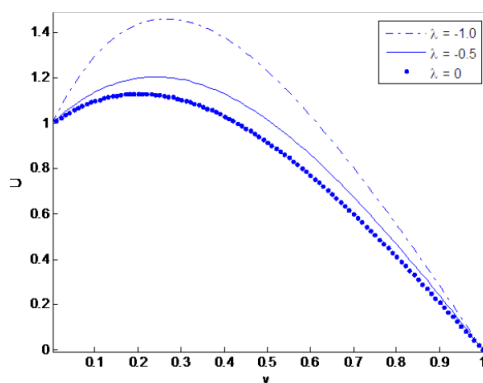


Fig. 5. Velocity profile for different values of  $\lambda$  ( $S = 2.0, Gr = 8.0$ )

Table 3. Estimated numerical values of mass flux  $Q$

S	$Gr = 5.0, \lambda = -0.3$	$Gr = 8.0, \lambda = -0.1$
	$Q$	$Q$
-1	0.64444	0.64513
-0.5	0.82778	0.83146
0.5	1.16111	1.18210
1	1.31111	1.41000

Table 4. Estimated numerical values of mean temperature  $\theta_m$

S	$Gr = 5.0, \lambda = -0.3$	$Gr = 8.0, \lambda = -0.1$
	$\theta_m$	$\theta_m$
-1	0.49416	0.40148
-0.5	0.55081	0.50380
0.5	0.67386	0.72479
1	0.74085	0.84436

Table 5. Comparison of numerical values between the present problem and of Jha and Ajibade (17)

S	Jha and Ajibade (17) $Gr = 8.0, y = 0.5$		Present work $Gr = 8.0, \lambda = 0, y = 0.5$	
	Temperature	Velocity	Temperature	Velocity
-1	0.56974696	1.05797571	0.56967230	1.05737847
-0.5	0.53296476	1.02743612	0.53289252	1.02736545
0.5	0.47029886	0.97521826	0.47029486	0.97528212
1	0.44340944	0.95272446	0.44348524	0.95321181

## 4 Conclusion

In this paper we have studied the effect of variable viscosity on natural convection flow between vertical parallel plates in the presence of heat generation/absorption, the work concluded that as the heat generation increases, fluid temperature and velocity increase while fluid temperature and velocity decreases with increase in heat absorption and also the velocity profile increases with increase in thermal buoyancy parameter. In addition, velocity decreases with the increase of the viscosity and hence reduced resistance to flow. Finally, it is concluded that the skin friction on both plates increase as viscosity increases.

## Competing Interests

Authors have declared that no competing interests exist.

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